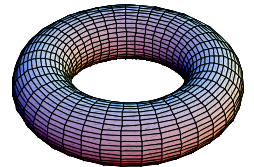


Adaptive Control of Feedback Linearizable Systems

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Outline

- Setup
- Ideal vs. actual control
- Affine systems
- Non-affine systems
- Example

Setup

- Parameter-dependent system reduce to normal form

$$\dot{\xi} = F(\xi, z, \mathcal{G})$$

$$\dot{z} = Az + E[\alpha(z, \mathcal{G}) + \rho(z, \mathcal{G})u]$$

$$y = Cz$$

- Design a feedback control that guarantees output stabilization $y \rightarrow 0$ for all \mathcal{G}

Ideal vs. Actual Control

- Ideal control is based on actual parameter

$$u^* = \rho^{-1}(z, \mathcal{G}) \{-\alpha(z, \mathcal{G}) + v\}$$

- Actual control is based on parameter estimate

$$u = \rho^{-1}(z, \hat{\mathcal{G}}) \{-\alpha(z, \hat{\mathcal{G}}) + v\}$$

System Dynamics with Actual Control

$$\dot{z} = Az + E \left[\alpha(z, \vartheta) + \rho(z, \vartheta)u \right]$$

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Ideal control

$$\dot{z} = Az + E[v + \Delta]$$

Actual control

$$\Delta = \left[\alpha(z, \vartheta) + \rho(z, \vartheta)u \right] - \left[\alpha(z, \hat{\vartheta}) + \rho(z, \hat{\vartheta})u \right]$$

Assumption 1: $\Delta(\xi, z, \hat{\vartheta}, \vartheta, u) = \Psi(\xi, z, \hat{\vartheta}, u)(\vartheta - \hat{\vartheta})$

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$$\dot{z} = A_c z + E\Psi(\vartheta - \hat{\vartheta})$$

Proposition 1

- Asymptotic output stabilization is achieved with the parameter estimator

$$\dot{\hat{\mathcal{J}}} = Q\Psi^T(\xi, z, \hat{\mathcal{J}}, u)E^T Pz, \quad Q = Q^T > 0$$

- Where P is the symmetric, positive definite solution of

$$A_c^T P + PA_c = -I$$

Proof of Prop 1

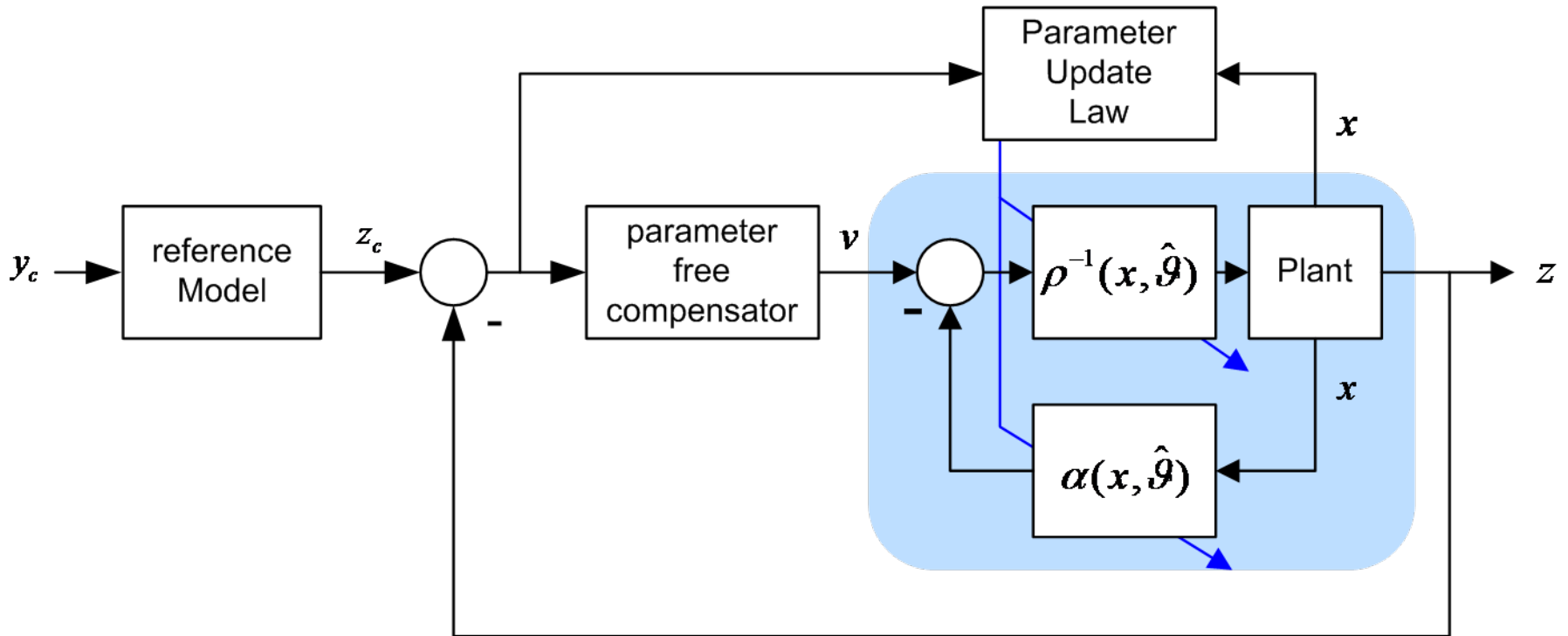
- Choose candidate Lyapunov function

$$V = z^T P z + (\mathcal{G} - \hat{\mathcal{G}})^T Q^{-1} (\mathcal{G} - \hat{\mathcal{G}})$$

- Compute

$$\begin{aligned}\dot{V} &= 2z^T P \dot{z} - 2\dot{\hat{\mathcal{G}}}^T Q^{-1} (\mathcal{G} - \hat{\mathcal{G}}) \\ &= z^T (P A_c + A_c^T P) z + 2 \left(z^T P E \Psi - \dot{\hat{\mathcal{G}}}^T Q^{-1} \right) \\ &= -z^T z\end{aligned}$$

Adaptive Control Structure



Example

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} x_2 \\ -0.2x_2 + x_1^3 / 2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} [u + \kappa x_1^3 + au]$$

$$\kappa \in [0, 1], \quad a \in [-0.1, 0.1]$$

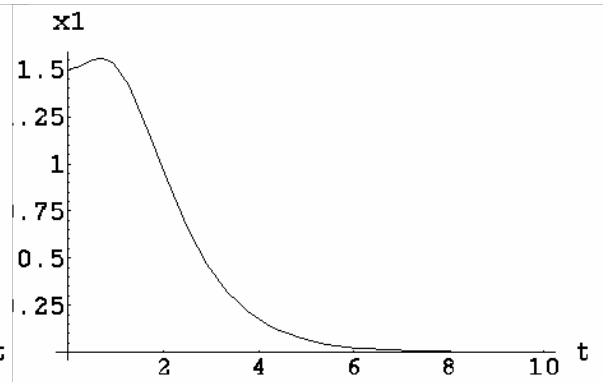
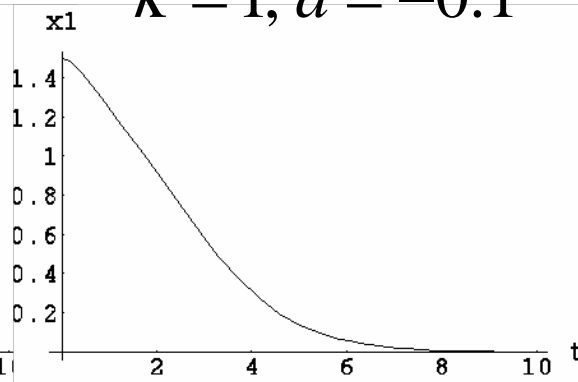
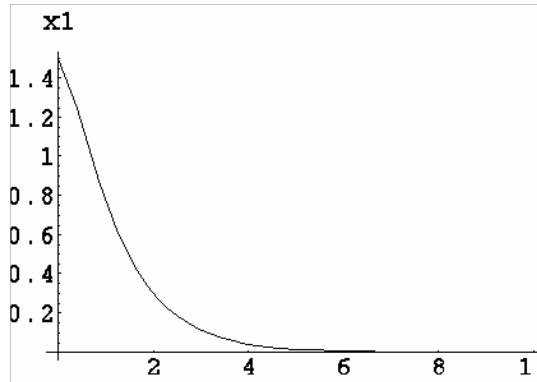
$$\alpha = -0.1x_2 + x_1 + x_1^3 / 2, \quad \rho = 1$$

$$u^* = \rho^{-1} \left(-\alpha + \begin{bmatrix} -1 & -2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} \right) = -2x_1 - 1.9x_2 - x_1^3 / 2$$

$$\Delta = (\kappa - \hat{\kappa}) x_1^3 + (a - \hat{a}) \left(-2x_1 - \frac{x_1^3}{2} - 1.9x_1 \right)$$

Example ~ Results

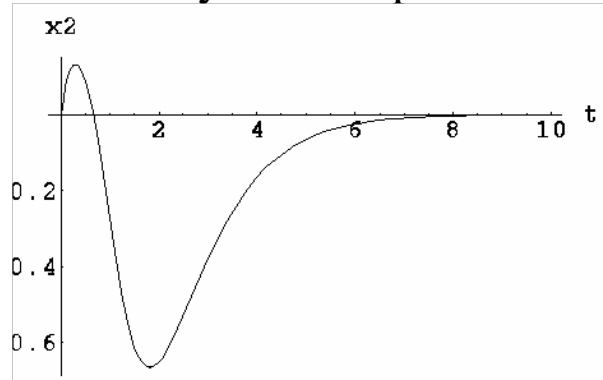
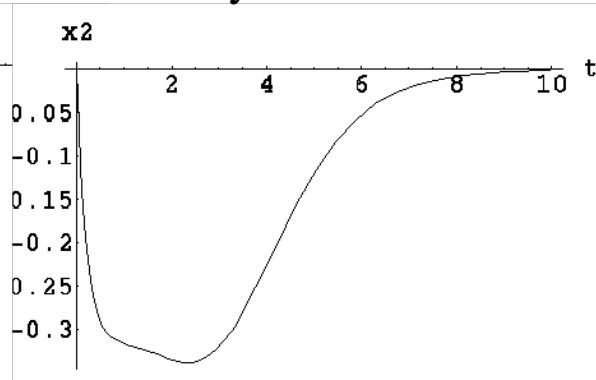
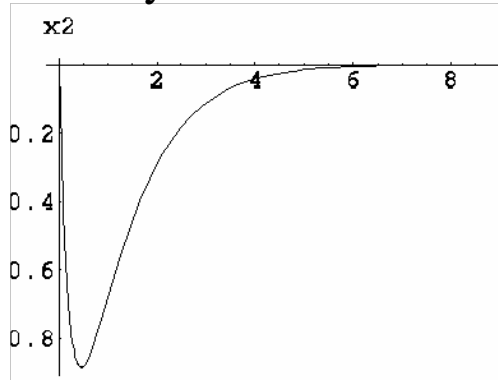
$$\kappa = 1, a = -0.1$$



nom system/nom control

actual system/robust control

actual system/adaptive control



Non-affine Systems

- Consider a system of the form

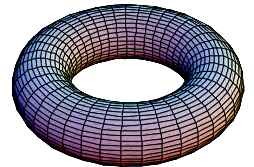
$$\dot{\xi} = F(\xi, z, \mathcal{G})$$

Non-affine part

$$\dot{z} = Az + E \left[\alpha(z, \mathcal{G}) + \rho(z, \mathcal{G}) \phi(u, \mathcal{G}) \right]$$

$$y = Cz$$

- The map ϕ is piecewise smooth and has a piecewise continuous inverse in u .



Ideal and Actual Controls

- The ideal control is

$$u = \phi^{-1}(\rho^{-1}(x, \mathcal{G})(-\alpha(x, \mathcal{G}) + v), \mathcal{G})$$

- The actual control is

$$\hat{u} = \phi^{-1}(\rho^{-1}(\hat{x}, \hat{\mathcal{G}})(-\alpha(\hat{x}, \hat{\mathcal{G}}) + Kz), \hat{\mathcal{G}})$$

Actual System Dynamics

- Again

$$\dot{z} = Az + E[v + \Delta]$$

- With

$$\Delta = [\alpha(x, \mathcal{G}) + \rho(x, \mathcal{G})\phi(u, \mathcal{G})] - [\alpha(\hat{x}, \hat{\mathcal{G}}) + \rho(\hat{x}, \hat{\mathcal{G}})\phi(u, \hat{\mathcal{G}})]$$

- Assumption

$$\Delta(\xi, z, \hat{\mathcal{G}}, \mathcal{G}, u) = \Psi(\xi, z, \hat{\mathcal{G}}, u)(\mathcal{G} - \hat{\mathcal{G}}) + \varphi_0(\xi, z, \hat{\mathcal{G}}, \mathcal{G}, u)$$

$$\varphi_0 \text{ bounded, } \mathcal{G}_{i,\min} \leq \mathcal{G}_i \leq \mathcal{G}_{i,\max} \quad i = 1, \dots, p$$

Adaptive Control

- Parameter update rule

$$\dot{\hat{\theta}} = \Omega \Psi^T (\xi, z, \hat{\theta}, u) E^T P z - \Omega \sigma(\hat{\theta})$$

- Where

$$(A + EK)^T P + P(A + EK) = -Q, \quad Q > 0$$

- and

$$\sigma(\hat{\theta}) = \begin{bmatrix} \sigma_1(\hat{\theta}_1) \\ \vdots \\ \sigma_p(\hat{\theta}_p) \end{bmatrix}, \quad \sigma_i(\hat{\theta}_i) := \begin{cases} \kappa_i & \hat{\theta}_i > \theta_{i_{\max}} \\ 0 & \theta_{i_{\min}} \leq \hat{\theta}_i \leq \theta_{i_{\max}} \\ -\kappa_i & \hat{\theta}_i < \theta_{i_{\min}} \end{cases} \quad \kappa_i > 0$$

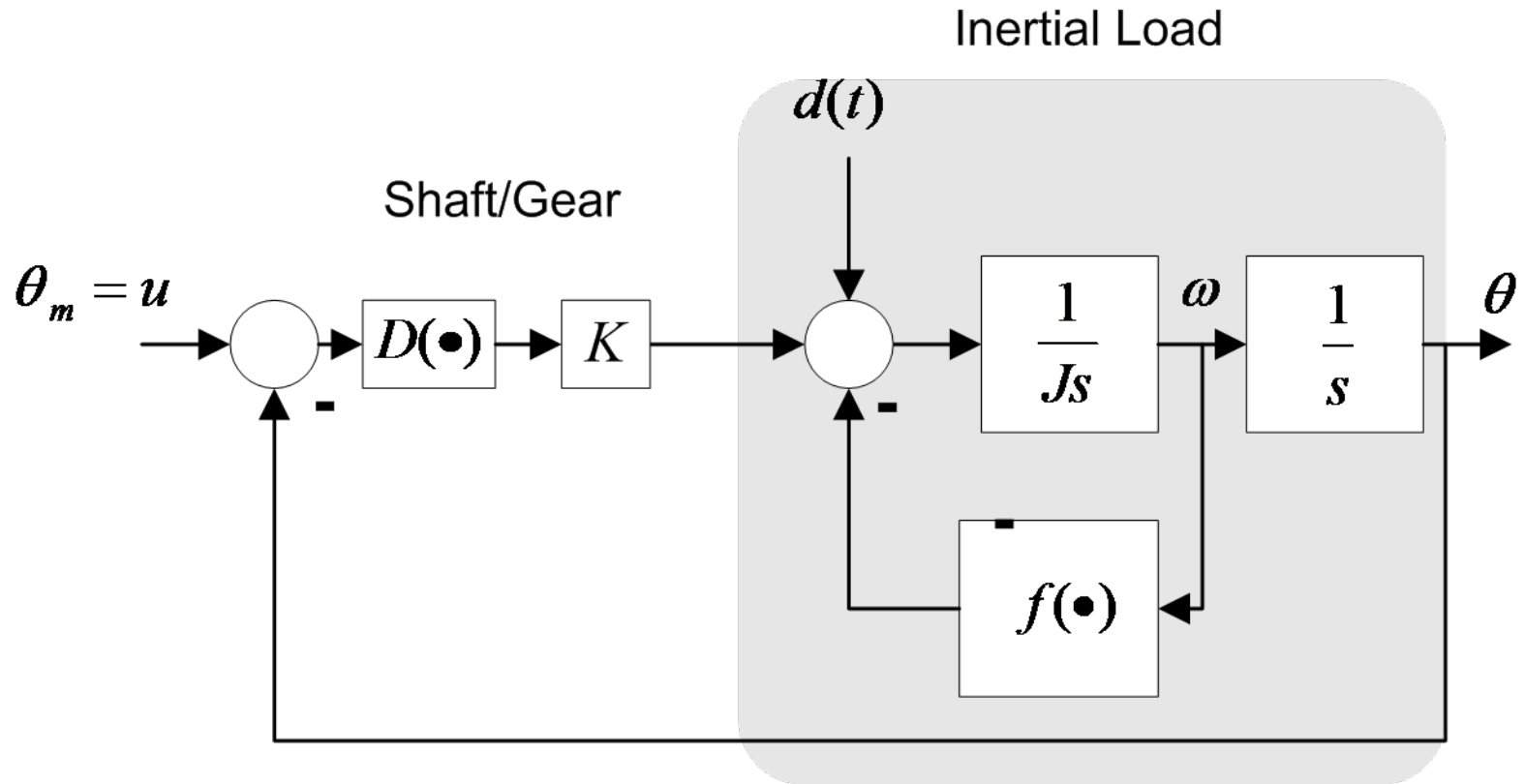
Proposition (output convergence)

- Define sets $S_{ext} = \left\{ (z, \mathcal{G}) \in R^{r+p} \left\| Q^{1/2} z - Q^{-1/2} PE\varphi_0 \right\|^2 > \left\| Q^{-1/2} PE\varphi_0 \right\|^2 \right\}$
 $S_{int} = \left\{ (z, \mathcal{G}) \in R^{r+p} \left\| Q^{1/2} z - Q^{-1/2} PE\varphi_0 \right\|^2 < \left\| Q^{-1/2} PE\varphi_0 \right\|^2 \right\}$

- Basic assumptions and (i) the only invariant set of closed loop on common set boundary corresponds to $z=0$, (ii) all trajectories that start in C_{param} remain in C_{param} .

$$\Rightarrow z(t) \rightarrow 0 \text{ as } t \rightarrow \infty$$

Example: drive with deadzone & friction



Model

$$T = K(\theta_m - \theta) \Rightarrow \theta_m = \frac{T}{K} + \theta$$

$$\dot{\theta} = \omega$$

$$\dot{\omega} = -f(\omega, b) + D(T, \varepsilon) + \kappa w(t)$$

$$f(\omega, b) = \begin{cases} b & \omega > 0 \\ -b & \omega < 0 \end{cases} = b \operatorname{sign}(\omega)$$

$$D(T, \varepsilon) = \begin{cases} x - \varepsilon & x \geq \varepsilon \\ x + \varepsilon & x \leq -\varepsilon \end{cases}$$

Controller ~ 1

- Dead zone inverse

$$D^{-1}(x, \varepsilon) = \begin{cases} x + \varepsilon & x > 0 \\ x - \varepsilon & x < 0 \end{cases}$$

- FBL

$$T = D^{-1}\left(-\sqrt{2}2\pi\omega - 2\pi\theta + f(\omega, b) - \kappa w(t), \varepsilon\right)$$

- Regressor

$$\Psi = -\left[\text{sign}(\omega) \quad \text{sign}(T) \quad -w(t)\right]$$

$$\Delta = \left[f(\omega, b) + D(T, \varepsilon) + \kappa w(t)\right] - \left[f(\omega, \hat{b}) + D(\hat{T}, \hat{\varepsilon}) + \hat{\kappa} w(t)\right]$$

$$f(\omega, b) - f(\omega, \hat{b}) = \text{sign}(\omega)(b - \hat{b})$$

etc.

Controller ~ 2 update law

$$A_c = \begin{bmatrix} 0 & 1 \\ -2\pi & -\sqrt{2}2\pi \end{bmatrix}, Q = \begin{bmatrix} 10 & 0 \\ 0 & 1 \end{bmatrix}$$

$$PA_c + A_c^T P = -Q$$

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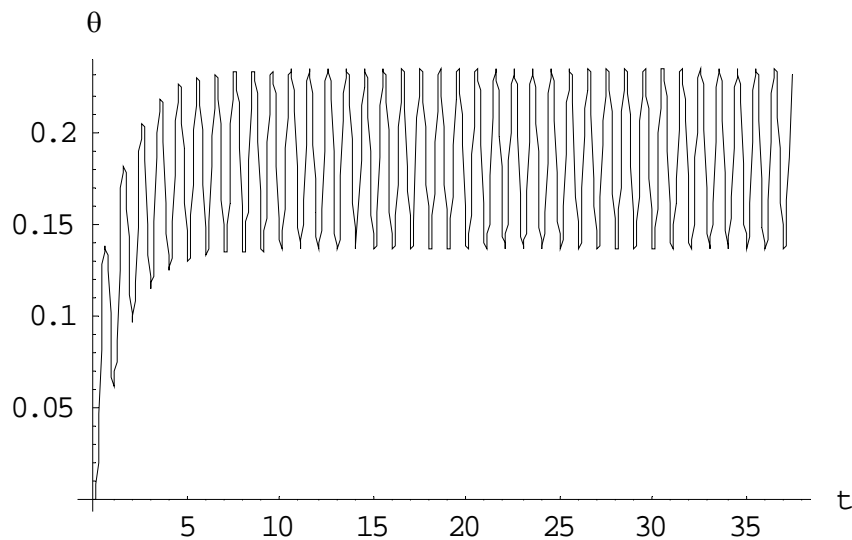
$$P = \begin{bmatrix} 7.986 & 7.958 \\ 7.958 & 0.1458 \end{bmatrix}, \lambda(P) = \{8.066, 0.06590\}$$

$$\frac{d}{dt} \begin{bmatrix} \hat{b} \\ \hat{\varepsilon} \\ \hat{\kappa} \end{bmatrix} = \Psi^T \begin{bmatrix} 0 & 1 \end{bmatrix} P \begin{bmatrix} \theta \\ \omega \end{bmatrix} - \begin{bmatrix} \sigma(\hat{b}, 1.5, 0) \\ \sigma(\hat{\varepsilon}, 1, 0) \\ \sigma(\hat{\kappa}, 2, -2) \end{bmatrix}$$

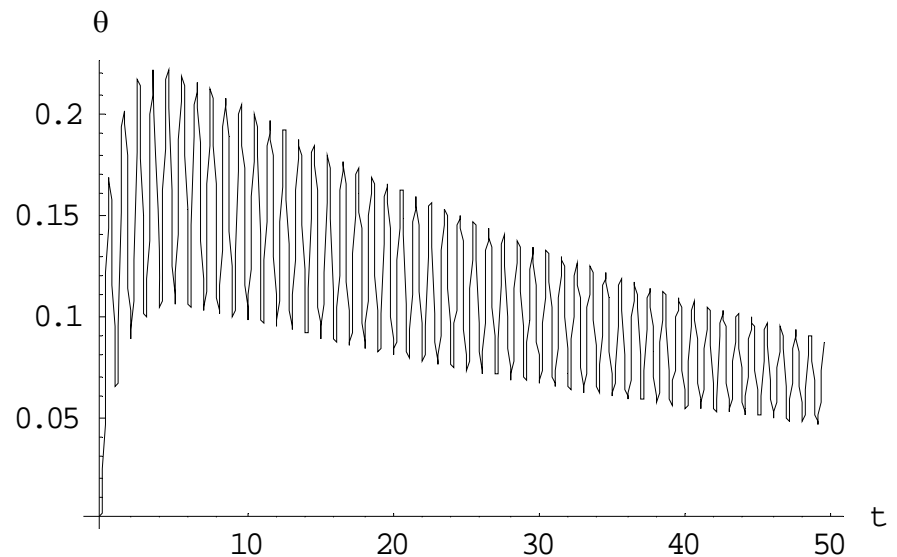
Simulation

$$b = 1, \varepsilon = 0.5, \kappa = 1 \quad \hat{b} = 0.9, \hat{\varepsilon} = 0.2, \hat{\kappa} = 0$$

$$w(t) = 1 + 4 \sin(2\pi t)$$



Simple linear stabilizer



Adaptive regulator